## The Tricritical Point in the n-C<sub>8</sub>H<sub>17</sub>SO<sub>3</sub>Na/ n-C<sub>4</sub>H<sub>9</sub>OH/H<sub>2</sub>O/n-C<sub>14</sub>H<sub>30</sub> System

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Synopsis. The phase behavior of three coexisting liquid phases has been studied in the four-component system of  $n\text{-}C_8H_{17}SO_3Na/n\text{-}C_4H_9OH/H_2O/n\text{-}C_14H_30$ . With a rise in the temperature, the three-phase region shrinks to a tricritical point at which the three liquid phases become identical.

Since ultralow interfacial tensions are attained and a solubilizing power of a surfactant reaches its maximum around a three-phase region (water(W), surfactant(D), and oil(O) phases)1,2) due to critical phenomena, it is very important to investigate the solution behavior of a surfactant around this region. In a three-liquid-phase system, two liquid phases (O-D or D-W phases) become identical in the presence of a third phase (W or O phase) at a critical end point which is located on the boundary between the two- and three-phase regions.2) If the two critical end points of the O-D and D-W phases coincide with each other, the three coexisting phases become identical at a highorder critical point, the tricritical point.3.4) This kind of critical phenomenon has been observed in some systems,5) but not in a surfactant system.

We previously found a tricritical phenomenon in a bile-salt system. In this paper, in order to find a tricritical point in an ordinary surfactant system, the phase behavior of the  $n\text{-}C_8H_{17}SO_3Na/n\text{-}C_4H_9OH/H_2O/n\text{-}C_{14}H_{30}$  system has been investigated.

## **Experimental**

Materials. Extra-pure-grade n-C<sub>8</sub>H<sub>17</sub>SO<sub>3</sub>Na and n-C<sub>14</sub>H<sub>30</sub> were obtained from the Tokyo Kasei Kogyo Co., while extra-pure-grade n-C<sub>4</sub>H<sub>9</sub>OH was obtained from the Wako Chemicals Co. The procedures for the determination of the phase beoundaries have been described elsewhere.<sup>4)</sup>

## **Results and Discussion**

In the  $n\text{-}\mathrm{C}_4\mathrm{H}_9\mathrm{OH/H}_2\mathrm{O}/n\text{-}\mathrm{C}_{14}\mathrm{H}_{30}$  system,<sup>6)</sup> a three-phase region appears at a lower temperature in the absence of a surfactant, as is shown in Fig. 1 ( $\odot$ ). In this case, a critical end point is an invariant point at a constant pressure (an atmospheric pressure).<sup>2,7)</sup> By adding  $n\text{-}\mathrm{C}_8\mathrm{H}_{17}\mathrm{SO}_3\mathrm{Na}$  to this three-component system, the maximum temperature of the three-phase region moves up to a higher temperature, as is also shown in Fig. 1 ( $\odot$ ). This maximum temperature of a three-phase region is determined for a variety of over-all compositions; the maximum over all compositions of these maxima may be identified as the tricriti-

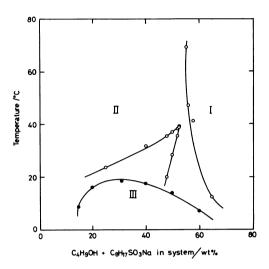


Fig. 1. Phase diagrams of equi-weight mixtures of H<sub>2</sub>O-C<sub>14</sub>H<sub>30</sub> containing C<sub>4</sub>H<sub>9</sub>OH (●) and 95 wt% C<sub>4</sub>H<sub>9</sub>OH+5 wt% C<sub>8</sub>H<sub>17</sub>SO<sub>3</sub>Na (○) as a function of temperature. I, II, and III denote one-, two-, and three-phase regions respectively.

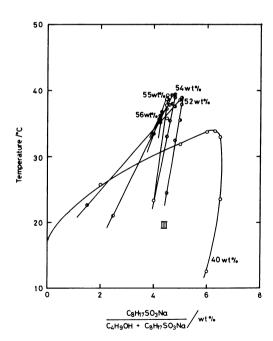


Fig. 2. The effect of concentration of  $C_8H_{17}SO_3Na$  in  $C_8H_{17}SO_3Na + C_4H_9OH$  on the three-phase region of equi-weight mixture of  $H_2O-C_{14}H_{30}$  containing  $C_8H_{17}SO_3Na + C_4H_9OH$ . Numerical number in the Figure indicates the concentration of  $C_8H_{17}SO_3Na + C_4H_9OH$  in system.

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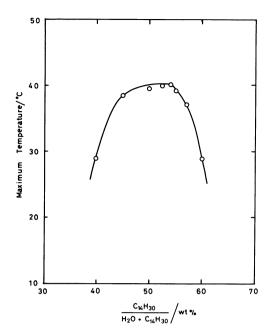


Fig. 3. The effect of H<sub>2</sub>O/C<sub>14</sub>H<sub>30</sub> ratio on the maximum temperature of the three-phase region.

cal point.3) This is because, in a four-component system, a line of critical end points exists in a certain space of temperature and compositions at a constant pressure, and the two critical end points of O-D and D-W exist at the respective temperatures as long as a three-phase region appears.4) Since a three-phase region is a point in a composition tetrahedron at the maximum temperature, the two critical end points may coincide at this point, i.e., the tricritical point. In Fig. 2, the three-phase region is determined as a function of  $n-C_8H_{17}SO_3Na/(n-C_8H_{17}SO_3Na+n-C_4H_{9}-$ OH) and the weight fraction of oil/water is unity. In this case, the maximum temperature of the three-phase region appears at the 54 wt%/system of  $(n-C_8H_{17}SO_3 Na+n-C_4H_9OH$ ). Similar maximum temperatures are determined for a variety of water/oil ratios and are plotted in Fig. 3. The maximum temperature of these maxima is 40.1 °C (n-C<sub>8</sub>H<sub>17</sub>SO<sub>3</sub>Na+n-C<sub>4</sub>H<sub>9</sub>OH, 56 wt%/system.  $n-C_{14}H_{30}/H_2O$ , 0.54/0.46 (W/W).  $n-C_{8}$ - $H_{17}SO_3Na/n-C_4H_9OH$ , 0.042/0.958 (W/W)).

Therefore, at this temperature, the three-phase re-

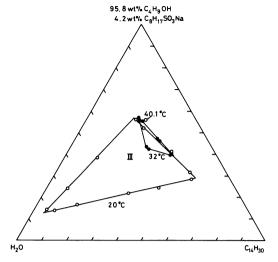


Fig. 4. The three-phase region of pseudo ternary system of (95.8 wt% C<sub>4</sub>H<sub>9</sub>OH+C<sub>8</sub>H<sub>17</sub>SO<sub>3</sub>Na)/H<sub>2</sub>O/C<sub>14</sub>H<sub>30</sub>. The three-phase region shrink to a tricritical point with the rise in temperature.

gion is a point in this four-component system and is identified as the tricritical point. In fact, the critical opalescence is observed in all phases in the vicinity of this point. The three-phase region in the pseudo-three-component system of 95.8 wt% n-C<sub>4</sub>H<sub>9</sub>OH+4.2 wt% n-C<sub>8</sub>H<sub>17</sub>SO<sub>3</sub>Na)/H<sub>2</sub>O/n-C<sub>14</sub>H<sub>30</sub> is shown at 20, 32, and 40.1 °C in Fig. 4. The three-phase region shrinks to a point on approaching 40.1 °C.

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